Phase-change materials (PCMs) are well-established categories of materials with many possible applications, ranging from the stabilization of temperature to heat or cold storage. The main principle of PCMs is the use of the latent heat of a phase change for energy storage. Although many pure chemical elements can be used as PCMs, a PCM very often consists of a number of substances. The main reason for creating a PCM as a mixture of various substances is to achieve a desirable melting temperature for a particular application. However, these mixed PCMs require accurate and reliable methods for determining their physical properties, since for numerical modeling the thermal properties of materials and their proper determination represent a significant issue that considerably affects the accuracy and credibility of numerical simulations and their outcomes.

The thermal properties of PCMs are usually obtained by differential scanning calorimetry (DSC), based on temperature and heat measurements of the investigated and reference materials. There are several approaches to modeling materials with phase changes. In this paper, the focus is on the enthalpy approach and the effective heat capacity method. Both techniques, which utilize the results from a particular DSC measurement, allow a treatment with the latent heat of a PCM and, as a result, the desired heat or cold storage may be effectively simulated. The presented methods were implemented using the results from DSC measurements in order to simulate a solar air collector with a PCM. The obtained results are presented and discussed. The paper also concerns the problems associated with the uncertainty of material properties and their influence on numerical simulations.

Keywords: phase change material (PCM), enthalpy method, effective heat capacity method, solar air collector

Materials with phase changes represent a significant issue that considerably affects the accuracy and credibility of numerical simulations and their outcomes. This is mainly due to the uncertainties associated with material properties and their influence on numerical simulations. In order to obtain accurate and credible results, it is essential to properly determine all thermal properties of materials and their proper estimation.

The optimal layout, usage, integration, and design of PCMs in buildings, constructions, and other equipment cannot be carried out without using numerical and computer simulations, optimization methods, and experimental measurements. In order to obtain accurate and credible results, it is essential to properly determine all thermal properties of the used materials and to precisely describe the operating conditions. For this purpose, differential scanning calorimetry (DSC) is very often used.
There are several methods and approaches as to how the materials embracing phase change and related phenomena can be modeled. In this paper the attention is focused on the enthalpy approach and the effective heat capacity method that enable the simulation of the heat transfer in materials with phase changes. As the inputs and parameters (e.g., the physical properties of a material) of the simulation the results from a DSC measurement may be utilized.

2 DIFFERENTIAL SCANNING CALORIMETRY

Differential scanning calorimetry is a thermo-analytical method and is widely used to assess and construct phase diagrams and to determine the thermophysical properties of materials, e.g., the crystallization and melting temperatures, heat capacity and the enthalpy.

The principle of differential scanning calorimetry is a measurement of the difference in the amount of heat needed to raise the temperature of the sample and the reference materials. The aim is to keep the temperature of both the sample and the reference materials at the same level during the experiment, while the temperature increases linearly. In order to precisely determine the properties and parameters of a sample material, the thermophysical properties of the reference material have to be known. The particular outcome of a DSC measurement for a PCM is shown in Figure 1.

3 ENTHALPY METHOD

The numerical modeling of PCMs requires solving the heat transfer problem in order to obtain the transient temperature distribution for the examined material. The heat transfer is described by the heat equation that is a partial differential equation of the second order:

$$\frac{\partial T}{\partial t} - \alpha \Delta T = 0$$  (1)

where $T$ (K) is the temperature, $t$ (s) is the time and $\alpha$ (m$^2$ s$^{-1}$) is the thermal diffusivity of the material.

The enthalpy method introduces the volume enthalpy $H/(J m^{-3})$, which includes the phase change phenomenon, to the equation since the enthalpy represents the sum of the sensible heat and the latent heat of the phase change. The function of the volume enthalpy is defined as follows:

$$H(T) = \int_0^T \left( \rho c - \rho L_i \frac{\partial s}{\partial T} \right) d\theta$$  (2)

where $\rho$ (kg m$^{-3}$) is the density, $c$ (J kg$^{-1}$ K$^{-1}$) is the specific heat, $L_i$ is the latent heat of the phase transformation and $s$ is the solid fraction. By substituting the enthalpy relation (2) into equation (1) we can obtain the reformulated equation describing the unsteady heat transfer in a material with phase changes:

$$\frac{\partial H}{\partial t} = \nabla \cdot (\lambda \nabla T)$$  (3)

where $\lambda$ (W m$^{-1}$ K$^{-1}$) is the thermal conductivity. As can be seen, in equation (3) there are two unknown quantities – the enthalpy and the temperature. However, they are coupled together through the enthalpy-temperature ($H$-$T$) relationship that can be obtained from a DSC measurement. An example of the $H$-$T$ relationship for a particular material with a phase change range from 25 °C to 27 °C is shown in Figure 2.

In order to solve equation (3) for a particular application the corresponding initial and boundary conditions have to be provided. To solve the system numerically, an appropriate numerical method is needed to assemble a system of discretized equations. For this purpose many numerical methods can be utilized, e.g., the finite-difference method, the finite-volume method, the finite-element method or the mesh-free methods. For simplicity, let us assume the finite-difference method. Thus, the partial derivatives in equation (3) are replaced by their finite-difference approximations and the original system is reformulated into a system of linear algebraic equations:

$$H_{i,j,k}^{n+1} = H_{i,j,k}^n + f(T_{i,j,k}^n, T_{i\pm h, j\pm k, k\pm h, \ldots})$$  (4)

However, due to the presence of unknown values of both the enthalpy and the temperature, the explicit scheme of the finite-difference method for the discretization in time has to be used. The temperature field is calculated in two successive steps: in the first step the enthalpy $H_{i,j,k}^{n+1}$ in time $t + 1$ is calculated from the known enthalpy and temperature values $H$, $T$ in time $t$ according to equation (4). After that the temperature $T_{i,j,k}^{n+1}$ in time $t + 1$ is calculated from the enthalpy $H_{i,j,k}^{n+1}$ according to the enthalpy-temperature relationship obtained, for instance, from a DSC measurement. Repeating the described procedure over all the time nodes leads to the targeted transient temperature field.
4 EFFECTIVE CAPACITY METHOD

The effective capacity method is based on the idea of incorporating the phase change phenomenon into the heat capacity calculations. This physical property represents the amount of heat needed for the matter to increase its temperature.

It means that the effective heat capacity $c_{\text{eff}}/(\text{J kg}^{-1} \text{K}^{-1})$ has to include the latent heat of the phase change. Therefore, the function of the effective heat capacity increases and decreases sharply with an apparent peak when the material undergoes the phase change. An example of the effective heat capacity function corresponding to the enthalpy curve is shown in the same Figure (Figure 2).

In order to calculate congruous and trustworthy results it is crucial to properly determine the effective heat capacity. For this purpose differential scanning calorimetry is one of the tools and techniques available.

By introducing the effective heat capacity, equation (1) becomes:

$$\rho c_{\text{eff}} \frac{\partial T}{\partial t} = \nabla(\lambda \nabla T)$$

In equation (5) there is only one unknown variable, the temperature $T$, and therefore a wider class of discretization approaches can be used. One of the most significant features is that the implicit scheme can be utilized. Hence, using the temperatures $T_n$ from the foregoing time step for the determination of the effective heat capacity in a successive time $n+1$, the discretized equation for each node $i, j, k$ can be written in the form:

$$f(T_{n+1}^{i,j,k}, T_n, \Delta x, \Delta y, \Delta z) = T_{n+1}^{i,j,k}$$

The system of algebraic equations can be assembled by using equation (6) applied to all the nodes of the discretized domain and an appropriate numerical method has to be used to solve it.

5 COMPARISON OF METHODS

The enthalpy method is based on the introduction of an additional quantity to the governing equation in order to include the phase change. From the computing point of view the volume enthalpy function introduces difficulties. Namely, (a) the desired quantity, i.e., the temperature, cannot be computed directly and the computation is split into two steps with an intermediate calculation, (b) the temperature search from a known enthalpy is demanding and requires a powerful search algorithm and (c) without additional techniques the explicit scheme, which is conditionally stable, must be used. The advantages of the enthalpy method are a better numerical stability when an explicit discretization scheme in time is used for both methods and its better accuracy in comparison with the effective heat capacity method.

The effective heat capacity method calculates the temperature field directly without intermediate steps and it allows the use of an implicit discretization scheme that is unconditionally stable. However, without additional techniques an assumption is required that the effective heat capacity is calculated using the temperature from a previous step. In the case that the effective heat capacity is a function of an unknown time, this makes the system of equations considerably more difficult to solve, and therefore the possibility of using an arbitrary time step (owing to the implicit scheme) is strictly confined. Moreover, when a problem with a large number of nodes (a 3D case with a large and intricate geometry) the computational demands of solving the system of equations becomes more arduous and time consuming.

6 RESULTS AND DISCUSSION

Both discussed methods were implemented in order to simulate and analyze the solar air collector, which is a solar thermal device that is used for heating in buildings. An issue with solar thermal systems is the general need for thermal storage in order to balance the heat demands over a certain time period. Therefore, the utilization of
phase change materials and their feature of energy storage can overcome the mentioned problem.

The TRNSYS software, which is a simulation tool designed for the analysis of transient systems, was used for modeling the solar air collector. Owing to the phase change material, in the case of the enthalpy method, the numerical model of heat transfer in a PCM has been implemented in MATLAB and both software packages, TRNSYS and MATLAB, were coupled together. In the case of the effective heat capacity method the numerical model of the PCM was implemented in the form of a stand-alone module (a DLL library) for TRNSYS in the programming language C++.

Both the software implementations utilized a result obtained from a DSC measurement of the PCM with the phase change temperature ranging from 30 °C to 38 °C and the latent heat of the phase change being 70 kJ kg⁻¹.

The simulations performed with the described methods produced comparable results. Figure 3 shows the outcomes of the simulation (meteorological data for 24 h in June, using the effective capacity method, the finite-difference discretization and the explicit scheme, the time step 2 seconds) for the so-called front-pass solar air collector that was split longitudinally into five separate sections. As seen in Figure 3 the courses of the PCM temperatures show the phase change in the given temperature ranges, the absorption and the release of the latent heat.

However, even though the material properties are properly determined by the DSC there are still quantities under uncertainty that may considerably influence the result of the simulations. A typical example is the heat transfer coefficient (HTC), since it can randomly fluctuate according to various factors. The HTC belongs to the class of operating conditions that can significantly affect the behavior of the system through the initial and boundary conditions. In order to properly solve the systems with parameters under uncertainty, additional techniques and methods, e.g., stochastic modeling and stochastic optimization, must be considered.

Moreover, the presented methods and their implementations can be utilized in a wide range of applications, e.g., for steel solidification and optimal control in the steel industry.

7 CONCLUSION

The presented paper introduces two possible approaches to modeling materials undergoing phase changes. Both techniques assume some particular thermophysical properties obtained, e.g., from the differential scanning calorimetry method. The concepts of the enthalpy approach and the effective heat capacity are described and the advantages, drawbacks and the usage are discussed.

The implemented methods were successfully tested on the simulation of the solar air collector with a PCM absorber. The obtained results suggest that the described approaches of numerical modeling and their implementations are valuable tools for solving problems in optimizing the design, usage and the integration of materials with phase changes.

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8 REFERENCES