MECHANICAL AND WETTING PROPERTIES OF NANOSILICA/EPOXY-COATED STAINLESS STEEL

Marjetka Conradi1, Gaber Intihar1, Milena Zorko2

1Institute of Metals and Technology, Lepi pot 11, 1000 Ljubljana, Slovenia
2National Institute of Chemistry, Hajdrihova 19, 1000 Ljubljana, Slovenia
marjetka.conradi@imt.si

Prejem rokopisa – received: 2015-03-13; sprejem za objavo – accepted for publication: 2015-04-03
doi:10.17222/mit.2015.060

1 INTRODUCTION

In recent decades, polymer composites have started to see uses in many applications as adhesives and matrix resins. Epoxy resin is one of the most common polymer matrices that are widely used to protect steel reinforcements in concrete structures1. It has excellent mechanical properties, chemical resistance, good electrical insulating properties, and in addition, it also provides an effective physical barrier between the metal and the environment containing an aggressive species, such as an enhanced chloride-ion concentration.

The practical use of epoxy coatings in industry, however, is seriously limited by their poor impact resistance and stress-cracking resistance due to a highly cross-linked structure2, as well as by their susceptibility to damage by surface abrasion and wear3. To overcome this drawback, researchers have made numerous attempts to improve the properties of epoxy by adding various nanofillers4–8. They studied the favourable effects of particle size, volume fraction and the quality of the dispersion on the mechanical properties of polymer composites9–14.

A lot of work has also been done in the field of modifying the surface wettability through the controlled tailoring of the surface morphology and the surface energy15,16. In this respect, the surfaces were coated with low-surface-energy compounds17 and/or their roughness was increased, i.e., by etching or nanoparticle deposition18,19. A further technological step is represented by the synthesis of superhydrophobic coatings inspired by
nature (i.e., the lotus leaf). Such coatings are a solution for corrosion, biofouling as well as water- and air-drag reduction applications. Additionally, they improve the mechanical characteristics of the surfaces. For example, nanosilica/epoxy coatings are increasingly attractive and have many potential applications in paints, coatings, sealants, adhesives, etc., due to their low cost, good adhesion to most substrates, good corrosion resistance, good scratch resistance, etc.13

Here, we investigate the influence of different sizes of silica nanoparticles (30 nm, 200 nm and 600 nm) on the surface morphology and mechanical characteristics of epoxy coatings on austenitic stainless steel of type AISI 316L. Through the implementation of silica nanoparticles into the epoxy matrix, we focus on a modification of the surface roughness of the epoxy coating that results, in combination with appropriate surface chemistry, in a significantly improved hydrophobicity.

2 EXPERIMENTAL

Materials. – Epoxy resin (Epikote 816, Momentive Specialty Chemicals B.V.) was mixed with a hardener Epikure F205 (Momentive Specialty Chemicals B. V.) in the mass ratio 100 : 53 % and used as the matrix in the composite. Composite-reinforcing silica (SiO$_2$) nanoparticles with mean diameters of 30 nm were provided by Cab-O-Sil, whereas 200 nm and 600 nm particles were synthesized following the Stöber–Fink–Böhm method in our laboratory20. Diglycidyl ether of bisphenol A (Sigma-Aldrich) was used as the silica-surface modifier to prevent agglomeration. Imidazole (Sigma-Aldrich) served as a reaction catalyst. Austenitic stainless steel of type AISI 316L was used as a substrate.

Surface modification of silica. – Silica and diglycidyl ether of bisphenol A were mixed in the mass ratio 2 : 3 and dispersed in 50 mL of toluene in the presence of imidazole (w = 25 %). The mixture was then refluxed at 100 °C for 2 h. To remove the by-product it was centrifuged three times using acetone as a solvent. The remaining silica was then dispersed in acetone and stirred at room temperature for 2–3 h. Finally, the silica was dried in an oven at 110 °C for 2 h.

Steel-substrate preparation. – The steel sheet with a thickness of 1.5 mm was cut into discs with diameters of 25 mm. Prior to the application of the coating, the steel discs were diamond polished following a standard mechanical procedure and then cleaned with ethanol in an ultrasonic bath.

Composite coating preparation. – Epoxy-based composites were prepared by blending with a mass fraction 2 % of 30 nm/200 nm/600 nm surface-modified SiO$_2$ particles. To improve the dispersion of the silica particles in the coating, they were dispersed in epoxy resin using acetone as a solvent. Prior to the addition of the silica particles, both the resin and the hardener were separately diluted in acetone in a mass ratio of 1 : 4. The nanoparticles were then dispersed in the epoxy resin/acetone solution using ultrasonification for 20–30 min at room temperature. After adding the hardener/acetone solution in the next step, the mixture was manually stirred for a 5 min. Finally, a drop 19 mg of the silica/epoxy resin/hardener/acetone mixture was poured onto the steel substrate disc and a uniform film was then applied to the substrate by a spin-coating process. The composite coatings were then cured in two steps: first pre-cured at 70 °C for 1 h and then post-cured at 150 °C for another hour. The resulting coatings on the steel-substrate plates were thick 300 nm, as determined by ellipsometry. For comparison, neat epoxy coatings without silica fillers were also prepared and cured in the same process as the composites. Finally, to additionally improve the non-wetting properties, the coatings were functionalized by dip-coating in ethanolic fluoroalkylsilane (FAS17, C$_{16}$H$_{33}$F$_{17}$O$_3$Si, Sigma-Aldrich).

Scanning electron microscopy (SEM). – SEM analysis using FE-SEM Zeiss SUPRA 35VP was employed to investigate the morphology of the silica/epoxy coatings’ surfaces.

Scratch test. – The scratch test was performed with a Revetest Scratch tester (CSM Instruments). In the experiment, a scratch length of 10 mm was made using a diamond tip and a linearly increased normal load from 1 N to 5 N at a speed of 5 mm/s. Four tests were performed per sample. A light microscope was employed to analyse the scratches.

Contact-angle and surface-energy measurements. – The static contact-angle measurements of water (W) on a clean AISI 316L diamond-polished sample and on the pure epoxy and silica/epoxy composite coatings prepared on an AISI 316L steel substrate were performed using a surface-energy evaluation system (Advex Instruments s. r. o.). Liquid drops of 5 μL were deposited on different spots of the substrates to avoid the influence of roughness and gravity on the shape of the drop. The drop contour was analysed from the image of the deposited liquid drop on the surface and the contact angle was determined by using Young-Laplace fitting. To minimize the errors due to roughness and heterogeneity, the average values of the contact angles of the drop were calculated approximately 30 s after the deposition from at least five measurements on the studied coated steel. All the contact-angle measurements were carried out at 20 °C and ambient humidity. As the contact angles were only available for water, an equation-of-state approach21,22 was used to calculate the corresponding surface energies.

Surface roughness. – A profilometer, model Form TalySurf Series 2 (Taylor-Hobson Ltd.), was employed for the surface analysis. The instrument has a lateral resolution of 1 μm and a vertical resolution of about 5 nm. It measures the surface profile in one direction. TalyMap gold 4.1 software was used for the roughness analysis. The software offers the possibility to calculate
the average surface roughness, $S_R$, for each sample, based
on the general surface-roughness equation:

$$S_R = \frac{1}{L_x} \frac{1}{L_y} \int_{-L_y/2}^{L_y/2} \int_{-L_x/2}^{L_x/2} |z(x, y)| \, dx \, dy$$

(1)

where $L_x$ and $L_y$ are the acquisition lengths of the
surface in the $x$ and $y$ directions and $z(x, y)$ is the height.
To level the profile, corrections were made to exclude
the general geometrical shape and possible measurement-induced misfits.

3 RESULTS AND DISCUSSION

3.1 Scratch resistance

Typical scratches in the 300 nm thick pure epoxy
coating and the 300 nm thick silica particles are presented in Figure 1.
The scratch profile as well as the resistance of the other silica/epoxy coatings is analogous to the 200 nm silica/epoxy coating under investigation, and thus not provided here. It is clear that there is much less displaced material in the case of the silica/epoxy coating compared to the pure epoxy coating. It also seems that the pure epoxy coating is much more brittle than the silica/epoxy coating. This, altogether, indicates that the embedded silica particles can improve the scratch resistance and enhance the toughness of the epoxy coating. In addition, the scratch-test results also suggest that the scratch resistance of the coatings is related to the interaction force between the coating and the steel substrate, which is apparently improved for the silica/epoxy coating.

3.2 Wetting properties

To analyse the surface wettability, five static contact-angle measurements with water ($W$) were performed on different spots all over the sample and used to determine the average contact-angle values with an estimated error in the reading of $(\theta \pm 1.0)^{\circ}$ and for the calculation of the surface energy. The wettability, however, was not possible to assess using non-polar liquids for the contact-angle measurements as they spread out on the coatings $(\theta \neq 0 \, ^{\circ})$. The contact angles and the surface energies for the epoxy and silica/epoxy coatings on the AISI 316L substrate in comparison to the clean, diamond-polished AISI 316L sample are reported in Table 1.

It was observed that all the investigated silica/epoxy coatings exhibited significantly higher values of static water-contact angles compared to the clean AISI 316L sample, as well as the AISI 316L substrate blended with pure epoxy. This suggests that the microstructure change of the epoxy coating upon adding the silica particles was reflected in an increased surface roughness, which is known to impart a hydrophobic effect to the surface.

The highest values of the static water angles, close to 120°, were however measured in the case of two types of silica/epoxy coatings: 200 nm silica/epoxy coatings and in case of silica/epoxy coatings filled with a combination of 30 nm and 600 nm silica particles. Possible reasons for this observation will be discussed in the following section on surface morphology and surface roughness.

Table 1: Surface properties of diamond-polished AISI-316L substrate and AISI 316L substrate when blended with pure epoxy and various types of silica/epoxy coatings. Static contact angles were measured with water ($\theta W$) and the corresponding surface energies were calculated using an equation-of-state approach.

<table>
<thead>
<tr>
<th>Substrate</th>
<th>Contact angle $\theta W$</th>
<th>Surface energy $\gamma W/(mN/m)$</th>
</tr>
</thead>
<tbody>
<tr>
<td>AISI</td>
<td>68.4</td>
<td>42.7</td>
</tr>
<tr>
<td>AISI + epoxy</td>
<td>80.2</td>
<td>35.4</td>
</tr>
<tr>
<td>AISI + 30 nm silica/epoxy</td>
<td>110.1</td>
<td>17.0</td>
</tr>
<tr>
<td>AISI + 200 nm silica/epoxy</td>
<td>117.7</td>
<td>12.8</td>
</tr>
<tr>
<td>AISI + 600 nm silica/epoxy</td>
<td>110.1</td>
<td>17.0</td>
</tr>
<tr>
<td>AISI + (30 + 200) nm silica/epoxy</td>
<td>111.7</td>
<td>16.1</td>
</tr>
<tr>
<td>AISI + (200 + 600) nm silica/epoxy</td>
<td>111.0</td>
<td>16.5</td>
</tr>
<tr>
<td>AISI + (30 + 600) nm silica/epoxy</td>
<td>118.4</td>
<td>12.5</td>
</tr>
</tbody>
</table>

As the contact angles were only available for water, an equation-of-state approach$^{11,22}$ was used to calculate the surface energies with Equation (1):

$$\cos \theta = 1 + 2 \sqrt{\frac{\gamma L}{\gamma W}} e^{-\beta (\gamma L - \gamma W)}$$

(2)

For a given value of the surface tension of the probe liquid $\gamma_1$ (i.e., for water $\gamma_1 = 72.8$ mN/m$^{24}$) and $\theta W$ measured on the same solid surface, the constant $\beta$ and

Figure 1: Light micrographs revealing the typical morphology of scratches: a) for the thick pure epoxy coating 300 nm on AISI 316L and b) for the thick epoxy coating 300 nm filled with silica particles 200 nm on AISI 316L.

Slika 1: Svetlobna mikroskopija prikazuje značilno morfologijo prask: a) na 300 nm debeli prevleki iz čiste epoksidne smole in b) na 300 nm debeli prevleki iz epoksidne smole, obogatene s silicijevimi delci 200 nm.
the solid surface-tension $\gamma$, values were determined using
the least-squares analysis technique. For the fitting with
Equation (2), a literature value of $\beta = 0.0001234$
($\text{mJ/m}^2$)$^{-2}$ was used, as weighted for a variety of solid
surfaces. Again, the calculated values of the solid
surface energy (Table 1) dropped significantly when the
clean AISI 316L substrate was covered with silica/epoxy
coatings, confirming the induced surface hydrophobicity.
The low surface energy of the silica/epoxy coatings is
most probably a consequence of the combination of
silica-induced surface roughness and the appropriate
surface chemistry due to the coatings' functionalization
with fluorooalkylsilane.

3.3 Surface morphology

Figure 2 compares the typical morphology of various
silica-epoxy coatings. It is clear that in spite of the
silica-surface modification with an epoxy-compatible
component, we could not prevent silica agglomeration in
the coating. After several different attempts we came to
the conclusion that the agglomeration appears during the
curing process and is most probably a consequence of
solvent (acetone) evaporation, together with the forma-
tion of a highly cross-linked epoxy structure.

A detailed look at the surface morphology, however,
brought us to the conclusion that there exists a typical
average agglomerate size, which depends on the size of
the silica fillers in the epoxy matrix. These agglomerates,
which are typically in the $\mu$m size range, consequently

Figure 2: SEM images of AISI 316L substrate when blended with: a) silica/epoxy 30 nm, b) silica/epoxy 200 nm, c) silica/epoxy 600 nm and d)
silica/epoxy coating (30 + 600) nm
Slika 2: SEM-posnetki podlage AISI 316L, prevklenje s prevlekami iz: a) 30 nm silicij-epoksidne smole, b) 200 nm silicij-epoksidne smole, c)
600 nm silicij-epoksidne smole in d) (30 + 600) nm silicij-epoksidne smole

Figure 3: Size distribution of silica agglomerates in 30 nm, 200 nm, 600 nm and (30 + 600) nm silica/epoxy coatings.
Slika 3: Velikostna porazdelitev silicijevih aglomeratov v prevlekah iz epoksidne smole, obogatene s silicijevimi nanodelci 30 nm, 200 nm,
600 nm in (30 + 600) nm
create a micro-roughness on top of the nano-roughness created by the individual silica nanoparticles embedded in the epoxy matrix. As is already known, it is the combination of the two, i.e., the micro- and the nano-roughness, that increases the static water contact angle and makes the surface more hydrophobic.25

As reported in Table 1, we measured the highest static water contact angles, close to 120 °, only on the surfaces of the 200 nm and (30 + 600) nm silica/epoxy coatings. In Figure 3 we can see that these two coatings are characterized mostly with agglomerates having diameters of 8 μm and 11 μm. The same holds for the morphology of the 30 nm silica/epoxy coating; however, here we also observe an considerable number of larger agglomerates that most probably influence the proper ratio between the micro- and nano-roughness necessary for an increase of the static water contact angle. This suggests the agglomerate/nanoparticle ratio is extremely sensitive to the appropriate surface roughness that will create a hydrophobic/superhydrophobic surface. This result also confirms the competitive importance of the surface morphology on the wetting properties compared to a low surface energy tailored with the surface chemistry.

3.4 Surface Roughness

Finally, we confirmed the morphology observations and determined the effect of the incorporation of silica on the morphology of the epoxy coating, by measuring the average surface roughness of the coatings, \( S_a \). An examination of the silica/epoxy-coated steel surface with a profilometer revealed that the nanoparticles’ size significantly influences the coating’s roughness and consequently the morphology of the surface. As listed in Table 2, \( S_a \) of 200 nm and (30 + 600) nm silica/epoxy coatings is of the same order of magnitude and in the intermediate regime compared to 30 nm and 600 nm silica/epoxy coatings. This is consistent with the observation of the average size of the agglomerates characterizing the morphology of each coating, as reported in the previous section. Here, we have shown that an intermediate roughness gives the best results in terms of an increased hydrophobicity (Tables 1 and 2). Moreover, this confirms the importance of the appropriate surface roughness on the wetting behaviour of the coatings.

Table 2: Average surface roughness, \( S_a \), of various silica/epoxy coatings on an AISI 316L substrate

<table>
<thead>
<tr>
<th>Substrate</th>
<th>( S_a )</th>
</tr>
</thead>
<tbody>
<tr>
<td>AISI + 30 nm silica/epoxy</td>
<td>0.65</td>
</tr>
<tr>
<td>AISI + 200 nm silica/epoxy</td>
<td>0.41</td>
</tr>
<tr>
<td>AISI + 600 nm silica/epoxy</td>
<td>0.27</td>
</tr>
<tr>
<td>AISI + (30 + 600) nm silica/epoxy</td>
<td>0.46</td>
</tr>
</tbody>
</table>

4 CONCLUSIONS

Nanosilica particles were homogeneously dispersed in an epoxy matrix at a mass concentration of 2% and mixtures with different combinations of 30 nm, 200 nm and 600 nm silica were successfully spin coated on austenitic stainless steel of type AISI 316L to form a 300 nm coating. For an additional improvement of the non-wetting properties, the coatings were functionalized by dip-coating in ethanolic fluorooalkylsilane (FAS17).

The mechanical properties of the coatings were evaluated with a scratch test, indicating that the more brittle pure epoxy coating underwent more severe damage, accompanied by a pronounced material displacement compared to the silica/epoxy coating. This indicates that the silica particles enhanced the toughness of the epoxy coating.

The silica nanoparticles changed the microstructure of the epoxy coating, which was reflected in an increased roughness of the silica/epoxy-coated AISI 316L sample. The increased hydrophobicity of the silica/epoxy coatings, on the other hand, was a consequence of the combination of silica-induced surface roughness and the appropriate surface chemistry, due to the coatings’ functionalization with fluorooalkylsilane.

The surface morphology of the silica/epoxy coatings was characterized by the formation of micrometre-size silica agglomerates as a consequence of the epoxy-matrix curing process. The significantly increased hydrophobicity in the 200 nm and (30 + 600) nm silica/epoxy coatings was connected to the proper combination of micro- and nano-roughness created by the agglomerates embedded in the epoxy matrix.

Acknowledgement

This work was carried out within the framework of the Slovenian programme P2-0132, “Fizika in kemija površin kovinskih materialov” of the Slovenian Research Agency, whose support is gratefully acknowledged by M. Conradi.

5 REFERENCES


Materiali in tehnologije / Materials and technology 49 (2015) 4, 613–618