1 INTRODUCTION

Alloys with the chemical composition close to SmCo$_{5-x}$ are used for fabricating the materials with a TbCu$_7$ meta-stable structure that cannot exist steadily. They are characterized by a high intrinsic coercivity temperature coefficient. The annealing process applied to these materials leads to the decomposition of the SmCo$_7$ phase into more stable structures, composed of the SmCo$_8$ and Sm$_2$Co$_{17}$ phases.

One of the most popular methods for determining the reversal-magnetization process is an analysis of recoil loops. Reversal magnetization in multiphase, nanocomposite permanent magnets, such as annealed Sm$_{12.5}$Fe$_8$Co$_{66.5}$Si$_2$Cu$_1$ ribbons, is very complex and often described with more than one type of process. On the basis of the recoil curves, the hysteresis loop was decomposed into the reversible and irreversible magnetization components. The decomposed curve was used to describe the processes that influence the reversal magnetization in the studied permanent magnets. Further, these components were used to model the recoil curves, using a modified hyperbolic $T(x)$ model based on the method described by Dospišál. The modeled hysteresis loop and recoil curves revealed a high compliance with the experimental data, proving the validity of the assumptions made in the modeling procedure.

Such information applied to hysteresis models can be used for simulating the major and minor hysteresis loops, the initial magnetization or recoil curves.

The aim of this paper is to present the theoretical description of the major hysteresis loop and recoil curves obtained using a hyperbolic $T(x)$ model modified by Dospišál and its comparison with the experimental data.

2 MATERIALS AND EXPERIMENTAL PROCEDURE

Samples of the Sm$_{12.5}$Fe$_8$Co$_{66.5}$Si$_2$Cu$_1$ alloy were obtained from high-purity elements, by arc melting, in a protective argon atmosphere. The studied ribbons were prepared by rapidly quenching the liquid alloy on a rotating copper wheel with a high linear velocity of 20 m/s. Both ingots and the samples were prepared in a protective gas atmosphere under a pressure of 0.4 × 10$^5$ Pa. The obtained ribbons were encapsulated in an argon atmosphere, annealed at 1123 K for 3 h and slowly cooled to room temperature.
XRD patterns were measured using a Bruker X-ray diffractometer equipped with a Lynx Eye semiconductor counter. Diffraction patterns were made using a Cu-Kα radiation source with a characteristic wave length of 0.1541 nm in the Bragg-Brentano geometry. The samples for the X-ray measurements were scanned in a 2Θ range from 30 ° to 120 ° with an angle step of 0.02 ° and an exposition time of 3 s. A quantitative and qualitative analysis of the phase composition was carried out using the Brass evaluation program applying the Rietveld profile-matching method.9

The major hysteresis loop and recoil curve were measured using a LakeShore VSM with the maximum external magnetic field of 2 T. The method of the recoil-curve decomposition into the constituent magnetization components was described elsewhere.10,11 The samples used for the magnetic measurements were in the form of ribbons of known dimensions. The demagnetization field resulting from their shape was taken into account and evaluated with the method described in15.

2.1 Hysteresis model

In the original T(x) model13,14 the hysteresis loop can be described with the sum of sigmoid and linear functions. The sigmoid hysteretic function characterizes the irreversible magnetization changes. The linear one is used for describing the reversible magnetization changes. In this research the authors used the T(x) model modified by Došpišel15,16 describing the reversible magnetization component with an anhysteretic sigmoid function. Based on this assumption, the whole reversal magnetization process was described with following Equations:

\[
f_{r,+,x}^{\text{hys}} = \mu_0 M_0 \sum_{n,j} B_{0,j} \left( \tanh[C_{0,j}(x-a_{0,j})] + b_{+,j} - b_{-,j} \right) \quad (1a)
\]

\[
f_{r,+,x}^{\text{anhys}} = \mu_0 M_{\text{max}} \sum_{n,j} \left( \frac{\tanh[C_{0,j}(x+a_{0,j})] + \tanh[C_{0,j}(x-a_{0,j})]}{2} \right) \quad (1b)
\]

\[
b_{+,j} = \tanh[C_{0,j}(x_k + a_{0,j})] - \tanh[C_{0,j}(x_k - a_{0,j})] \quad (1c)
\]

\[
f_{r,+,x}^{\text{hys}} = \mu_0 M_0 \sum_{n,j} B_{0,j} \left( C_{0,j}(x+a_{0,j}) + b_{+,j} + b_{-,j} \right) \quad (2a)
\]

\[
f_{r,+,x}^{\text{anhys}} = \mu_0 M_{\text{max}} \sum_{n,j} \left( \frac{\tanh[C_{0,j}(x+a_{0,j})] + \tanh[C_{0,j}(x-a_{0,j})]}{2} \right) \quad (2b)
\]

\[
b_{-,j} = \tanh[C_{0,j}(x_k - a_{0,j})] - \tanh[C_{0,j}(x_k + a_{0,j})] \quad (2c)
\]

\[
b_{1,1} = \frac{\tanh[C_{0,j}(x_m + a_{0,j})] - \tanh[C_{0,j}(x_m - a_{0,j})]}{2} \quad (3)
\]

where (+) and (−) in the \( f_{r,+,x}^{\text{hys, anhys}} \) functions represent the ascending and descending changes of the reversible (anhys) and irreversible (hys) components, respectively; \( x \) is the external-magnetic-field excitation, \( a_{0,j} \) is the center of the \( j \)th pinning/nucleation site, \( a_{0,j} \) is the center of the \( j \)th reversible process; \( B_{0,j}, B_{0,i} \) are the amplitudes of the \( j \)th and \( i \)th magnetization components; \( C_{0,j}, C_{0,i} \) are the sheering factors, while \( x_m \) represents the maximum-external-magnetic-field excitation. The \( i \) and \( j \) indexes refer to individual reversible and irreversible magnetization components, respectively, and \( n_{\text{irr,rev}} \) is their total number.16

3 RESULTS AND DISCUSSION

Figure 1 presents the experimental X-ray diffraction pattern compared with the results of the Rietveld refinement simulation, obtained for the annealed Sm12.5Fe8Co66.5Si2Cu11 thin ribbons.

![Figure 1: X-ray diffraction patterns: measured and calculated from the Rietveld refinement and the difference curve for a Sm12.5Fe8Co66.5Si2Cu11 ribbon annealed at 850 °C for 3 h](image)

Slika 1: Rentgenogram, izmerjen in izračunan iz Rietveldovega približka, ter diferencijska krivulja za trak Sm12.5Fe8Co66.5Si2Cu11, žarjen 3 h na 850 °C

![Figure 2: Measured demagnetization curve and the calculated hysteresis loop, obtained with the modified T(x) model, for the Sm12.5Fe8Co66.5Si2Cu11 ribbon annealed at 850 °C for 3 h](image)

Slika 2: Izmerena krivulja razmagnetenja, izračunana z modifikiranim modelom \( T(x) \) histeretike zanke za trak Sm12.5Fe8Co66.5Si2Cu11, žarjen 3 h na 850 °C
According to the Rietveld refinement, it was found that the studied alloy was composed from Sm$_2$Co$_{17}$ (22.92 %), SmCo$_5$ (37.45 %) and SmCo$_5$ (39.63 %) phases. A lack of one of the less intense peaks on the experimental diffraction pattern, as compared with the simulation, can be associated with the preferred position, occupied by the Cu atoms in the TbCu$_7$ structure and the use of a copper X-ray source. Due to the overlapping peaks, originating from the presence of different crystaline phases, it was not possible to estimate the average grain size using the Bragg equation. However, it was possible to state that it was less than about 120 nm.

With the measured demagnetization curve and the simulated one, obtained with the modified hyperbolic $T(x)$ model, the major hysteresis loop is presented in Figure 2.

The experimentally determined hysteresis loop was used to estimate the basic magnetization parameters: saturation of the magnetization $\mu_0M_s (0.90 \, \text{T})$, remanence $\mu_0M_r (0.70 \, \text{T})$ and coercivity $H_C (0.41 \, \text{T})$.

The saturation of the magnetization and the remanence were also compared with those calculated from the initial magnetization curve and the irreversible magnetization dependence after the extrapolation to the infinite field, using the method described elsewhere. The calculated parameters were as follows: $\mu_0M_s(\infty) = 0.91 \, \text{T}$ and $\mu_0M_r(\infty) = 0.70 \, \text{T}$; they were used to obtain the $M_s(\infty)/M_r(\infty)$ ratio which was 0.77.

On the basis of the $M_s(\infty)/M_r(\infty)$ ratio combined with the shape of the demagnetization curve and the estimated grain size, it was possible to conclude which type of interactions between the particles is dominant. According to the literature, a multiphase material with a smooth demagnetization curve as observed on Figure 2 and the value of the $M_s/M_r$ ratio higher than 0.5 is characteristic for exchange-coupled nanocomposites and/or anisotropic permanent magnets.

The measured demagnetization curve (the lower arm of the hysteresis is symmetric) was compared with the theoretically simulated hysteresis loop (Figure 2). The simulation was done using the Mathematica software and Equations (1) to (3). The obtained results showed a high compliance with the experiment.

The startup data for simulating the major hysteresis loop and recoil curve was determined on the basis of the data obtained from the analysis of the reversible and irreversible magnetic susceptibilities (Figure 3).

As it can be seen on Figure 3, both reversible and irreversible susceptibilities are composed of at least three distribution sites. The fitting parameters determined from susceptibility curves are gathered in Table 1.

In order to simulate the irreversible magnetization changes, it was necessary to use a combination of three hysteretic functions, properly representing three pinning/nucleation sites. On the other hand, the reversible magnetization was represented by a combination of three anhysteretic functions, sourcing from the rotation of magnetization vectors, the free domain-wall movement of unpinned domain walls or the bowing of strongly pinned domain walls.

### Table 1: Fitting parameters used in the simulation of the major hysteresis loop and recoil curve applying the modified $T(x)$ model, where: $a_{th}$ – the center of the $i^{th}$ pinning/nucleation site (irreversible) or the peak resulting from the reversible process, $B_{th}$ – the amplitude of the $i^{th}$ magnetization component, $C_{th}$ – the shearing factor of the $i^{th}$ magnetization component

<table>
<thead>
<tr>
<th>Component</th>
<th>$a_{th}$</th>
<th>$B_{th}$</th>
<th>$C_{th}$</th>
</tr>
</thead>
<tbody>
<tr>
<td>rev</td>
<td>1</td>
<td>2.705</td>
<td>0.001</td>
</tr>
<tr>
<td></td>
<td>2</td>
<td>0.107</td>
<td>0.320</td>
</tr>
<tr>
<td></td>
<td>3</td>
<td>0.114</td>
<td>1.200</td>
</tr>
<tr>
<td>irr</td>
<td>1</td>
<td>0.039</td>
<td>0.022</td>
</tr>
<tr>
<td></td>
<td>2</td>
<td>5.618</td>
<td>0.413</td>
</tr>
<tr>
<td></td>
<td>3</td>
<td>2.672</td>
<td>0.749</td>
</tr>
</tbody>
</table>

Figure 3: Reversible, irreversible and total susceptibilities determined from the magnetization components for a Sm$_{12.5}$Fe$_5$Co$_{66.5}$Si$_2$Cu$_{11}$ ribbon annealed at 850 °C for 3 h.

Slika 3: Reverzibilna, irreverzibilna in skupna občutljivost, določena iz komponent magnetizacije za trak Sm$_{12.5}$Fe$_5$Co$_{66.5}$Si$_2$Cu$_{11}$, žarjeni 3 h na 850 °C

Figure 4: Decomposition of the hysteresis loop simulated with the modified $T(x)$ model into the hysteretic and anhysteretic functions

Slika 4: Razstavljanje z modificiranim modelom $T(x)$ simulirane histerezne zanke v hysteretno in anhisteretno funkcijo
The decomposition of the hysteresis loop into the hysteretic and anhysteretic curves, representing irreversible and reversible magnetization processes, respectively, is presented in Figure 4.

The obtained results were also used for simulating the recoil curve in the demagnetization direction by applying Equations (1) to (3). The comparison of the simulated and measured recoil curves is presented in Figure 5.

As can be seen in Figure 5, the simulated and measured curves are similar. The observed small differences between the experiment and the simulation can be related to the recoil-loop openness effect that is, in turn, associated with the magnetic viscosity.

4 CONCLUSION

From the X-ray diffraction it was found that the studied sample was composed of three different phases, i.e., \(Sm_{12.5}Fe_8Co_{66.5}Si_{2}Cu_{11}\) ribbon annealed at 850 °C for 3 h. The observed small difference in the value of the aforementioned ratio is typically met in the samples characterized by a high anisotropy\(^{20}\) or strong exchange coupling between nanosized grains.\(^{18,19}\) The multiphase composition combined with a smooth, single-step demagnetization curve can be treated as a proof of strong exchange coupling between the grains of the constituent phases.\(^{21}\)

The decomposition of the demagnetization curve into the reversible and irreversible magnetization components provided information on the quantity and type of the reversal-magnetization processes occurring in the studied material. Furthermore, using the obtained results and the \(T(x)\) model modified by Dospial, it was possible to determine the anhysteretic and hysteretic curves forming the hysteresis. The same data was used to simulate the recoil curve that showed a high compliance with the experimentally obtained one.

Acknowledgement

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5 REFERENCES


Figure 5: Comparison of the measured and simulated, with the modified \(T(x)\) model, recoil loops for the Sm12.5Fe8Co66.5Si2Cu11 ribbon annealed at 850 °C for 3 h.

Slika 5: Primerjava izmerjenih in z modificiranim modelom \(T(x)\) simuliranih povratnih krivulj za trak Sm12.5Fe8Co66.5Si2Cu11, žaren 3 h na 850 °C.
17 H. Zijlstra, Experimental methods in magnetism, Elsevier North-Holland, Amsterdam 1967